

# **Analysis of Intermodulation Distortion in Ferrite Circulators**

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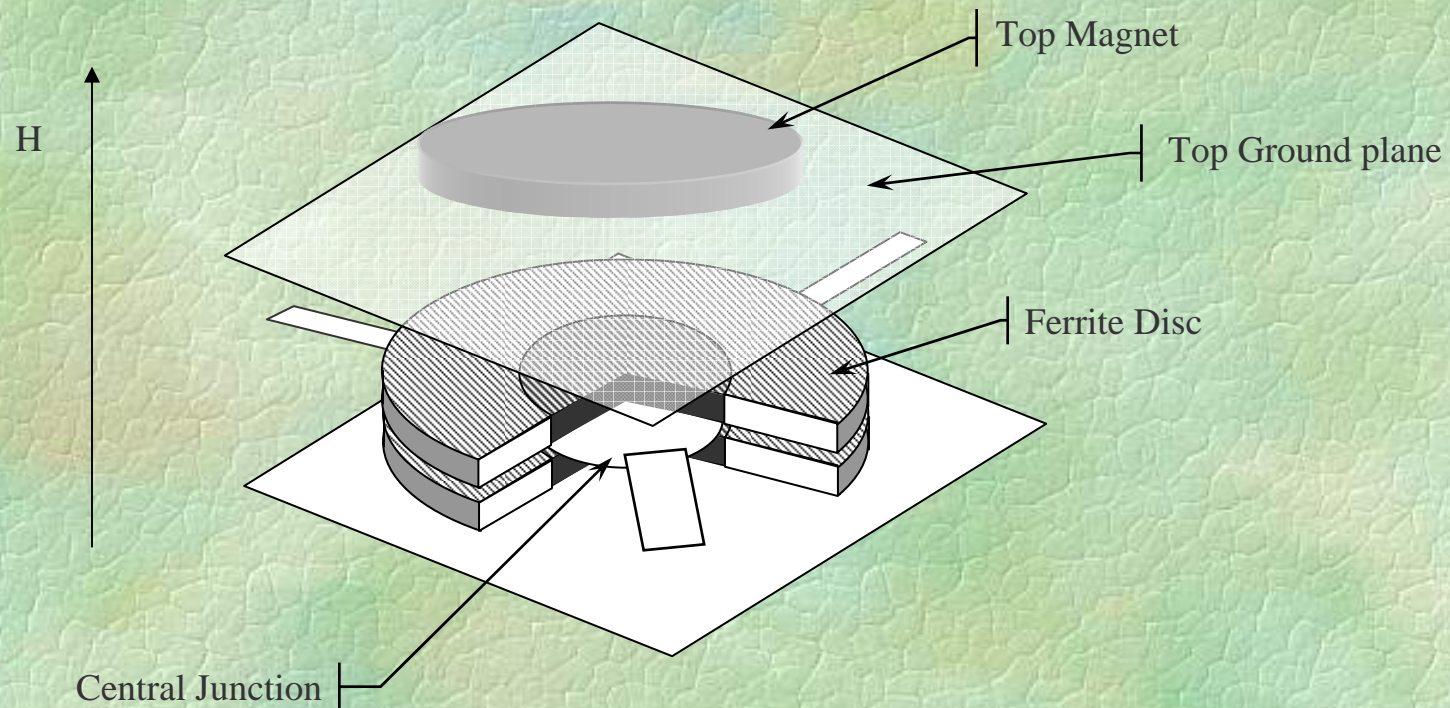
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**Harvard, MA**

# OVERVIEW

- **Introduction**
- **Linearized Equation of Motion for Magnetization**
- **Nonlinear Oscillations of Magnetization**
- **Nonlinear Model**
- **IMD Data on a PCS Circulator**
- **Summary**

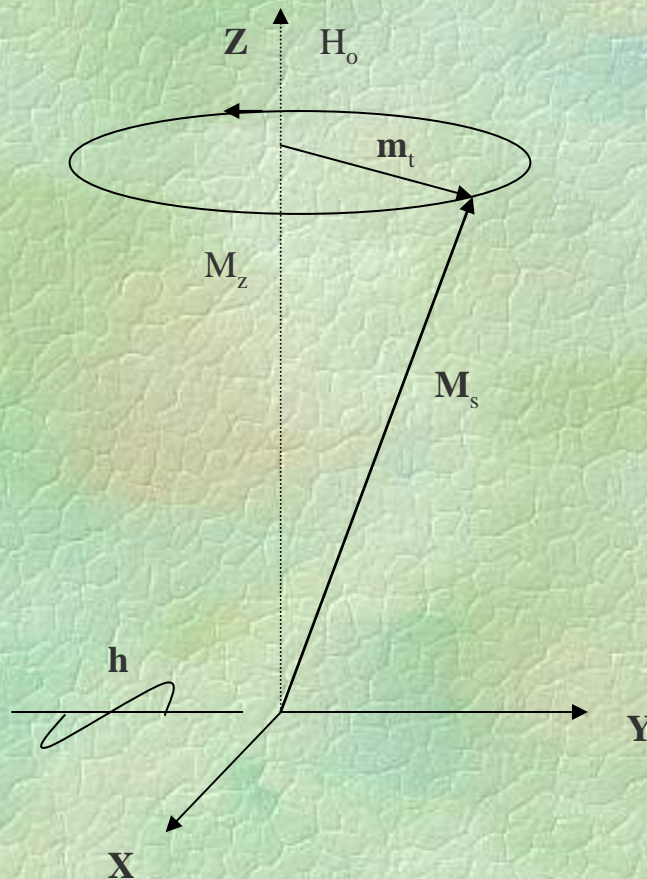
## Basic Construction of a Stripline Ferrite Junction Circulator



**OBSERVATION:** As  $H$  was increased, 3<sup>rd</sup> order IMD reduced considerably.

# Equation of Motion of Magnetization Vector

## Linear Theory



$$\frac{d\mathbf{M}_s}{dt} = -\gamma(\mathbf{M}_s \times \mathbf{H})$$

$$\mathbf{M}_s = \mathbf{M}_z + \mathbf{m}_t \quad \mathbf{H} = \mathbf{H}_0 + \mathbf{h}$$

$$h \ll H_0 \quad m_t \ll M_z$$

Assuming rf products ( $hm_t$ )  $\sim 0$

$$\frac{dm_t}{dt} + \gamma(m_t \times H_0) = -\gamma(M_z \times h)$$

## Solution of Linearized Equation of Motion

Assuming harmonic ( $\exp(i\omega t)$ ) time dependence of  $\mathbf{h}$  and  $\mathbf{m}_t$ :

$$i\omega m_x + \gamma H_o m_y = \gamma M_z h_y$$

$$i\omega m_y - \gamma H_o m_x = -\gamma M_z h_x$$

$$i\omega m_z = 0$$

Solution:

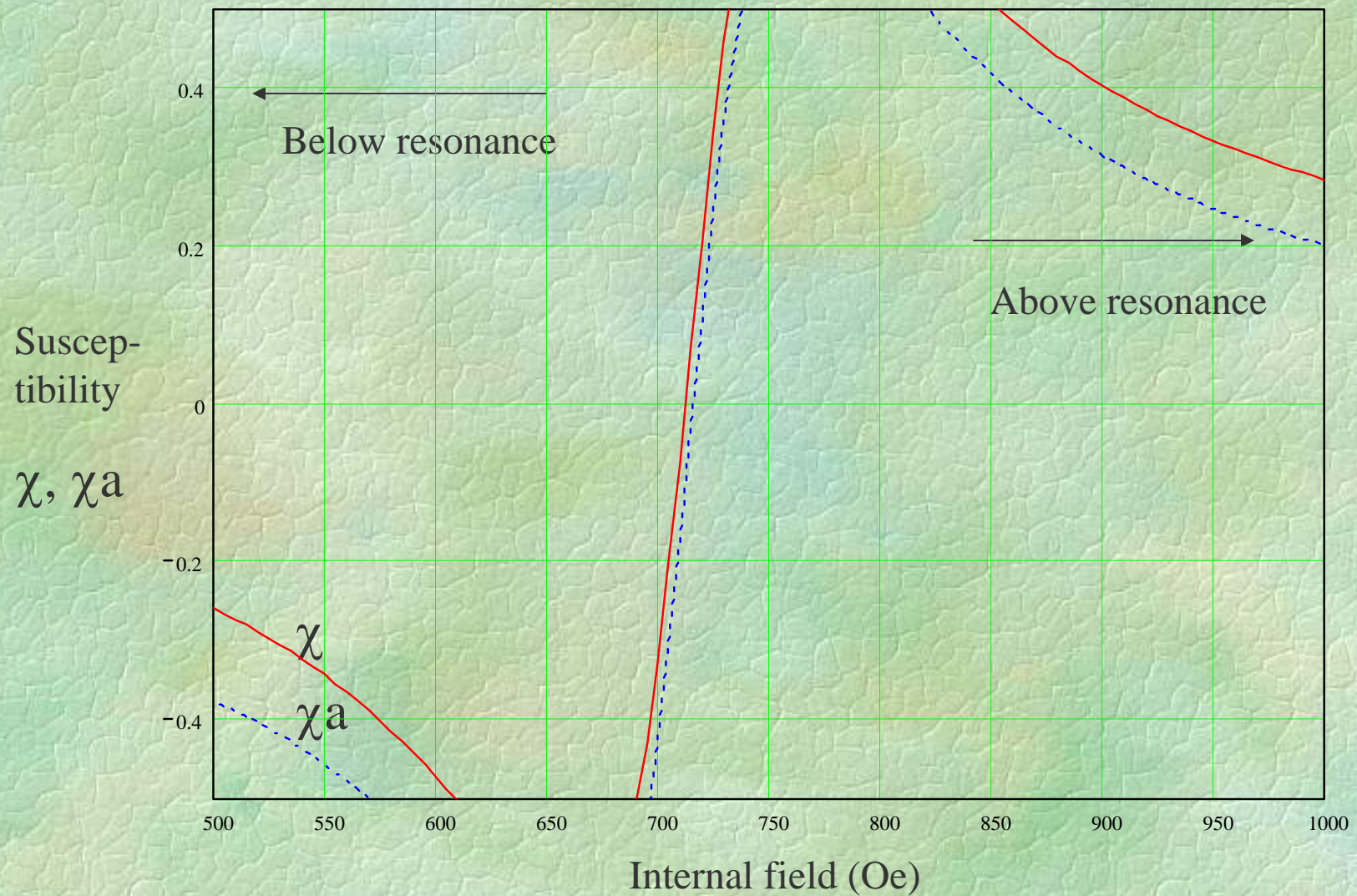
$$m_x = \chi h_x + i\chi_a h_y \quad m_y = \chi h_y - i\chi_a h_x \quad m_z = 0$$

$$\chi = \frac{\gamma M_z \omega_o}{\omega_o^2 - \omega^2}$$

$$\chi_a = \frac{\gamma M_z \omega}{\omega_o^2 - \omega^2}$$

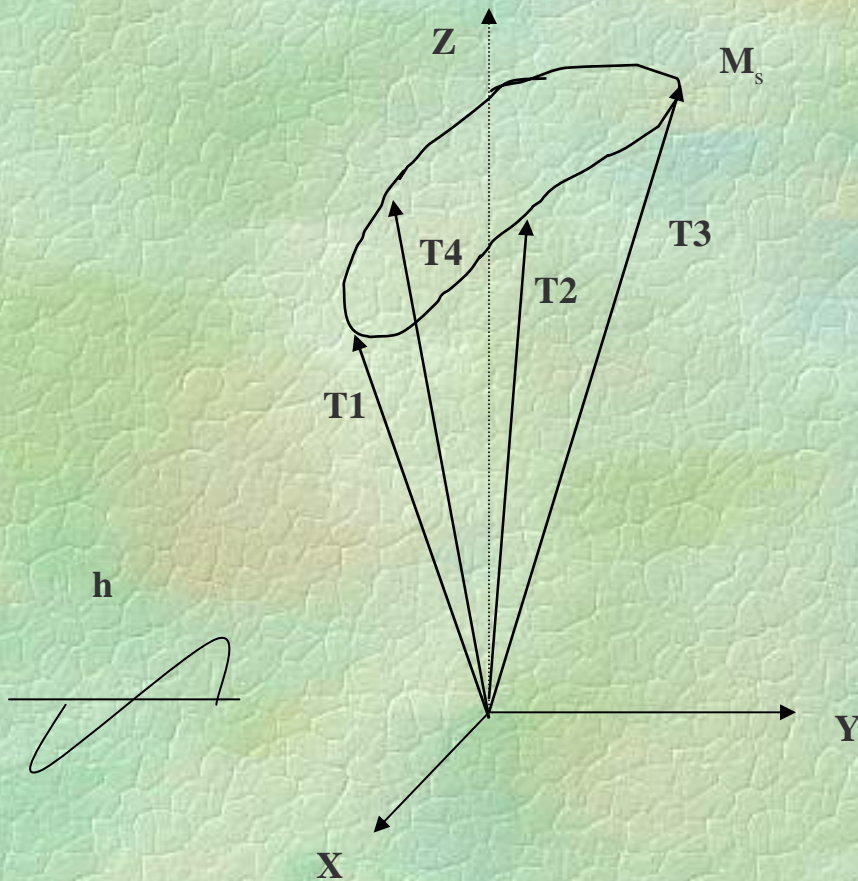
**Ferromagnetic resonance:**  $\omega_o = \gamma H_o$

# Tensor Susceptibility vs. Internal Field



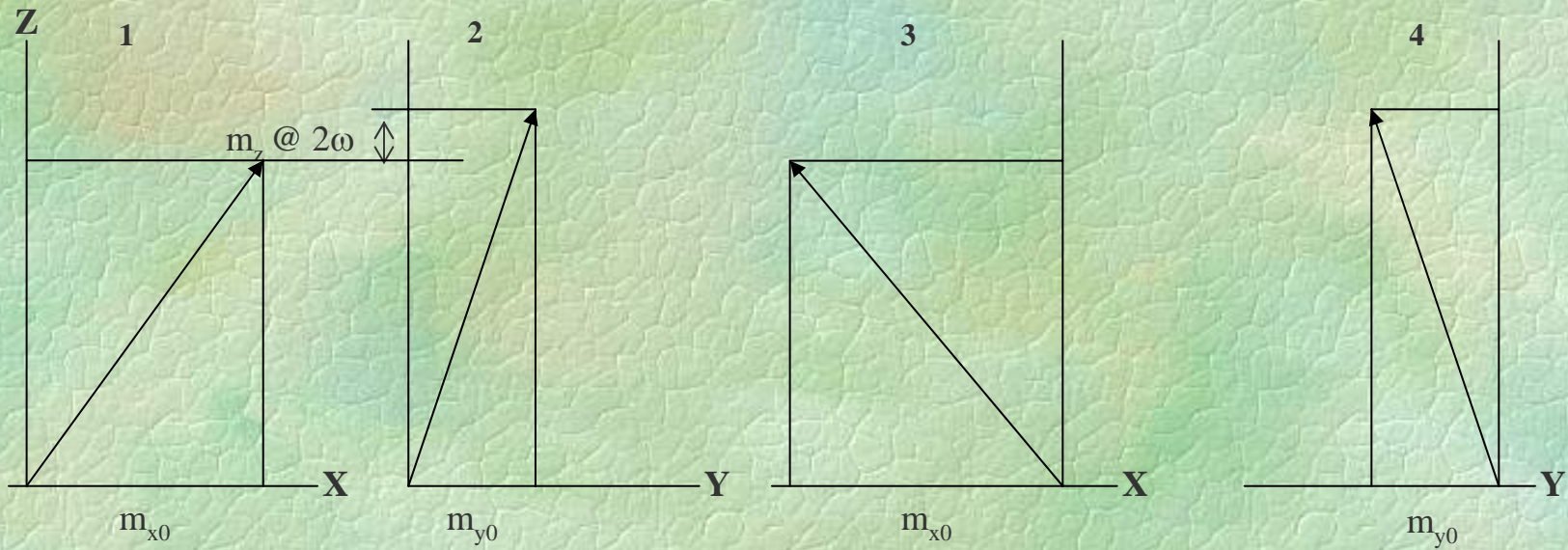
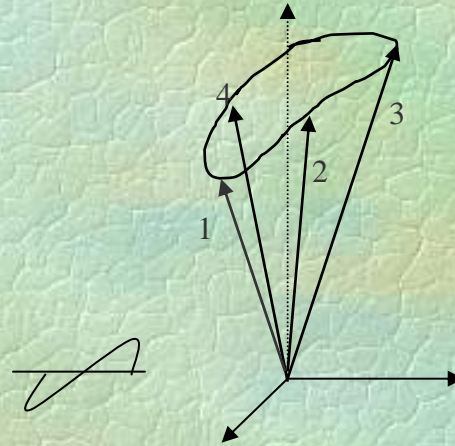
**Difference between  $\chi$  and  $\chi_a$  is more in the below resonance than above resonance region**

# Nonlinear Oscillations of Magnetization



- Magnetization vector does not precess in a circular path.
- As the rf power is increased, higher order terms become significant and can no longer be neglected. Time derivative of  $m_z$  is not zero.
- Instability in the non-linear motion at high power levels depends on the anisotropy (shape, magneto-crystalline) present in the sample.

# Harmonic Generation



**Note: Magnetization  $M_s$  is held constant**

## Nonlinear Model

- Small signal approximation:

$$m_x = \chi h_x + i\chi_a h_y \quad m_y = \chi h_y - i\chi_a h_x \quad m_z = 0$$

- High signal levels (for linearly polarized rf fields):

$$m_x = \chi h_x \quad m_y = -i\chi_a h_x$$

$$m_t^2 = m_x^2 + m_y^2 = h_x^2 \left[ (\chi^2 - \chi_a^2) \left( \frac{1 - \cos(2\omega t)}{2} \right) + \chi_a^2 \right]$$

$$M_s^2 = (M_z + m_z)^2 + m_t^2$$

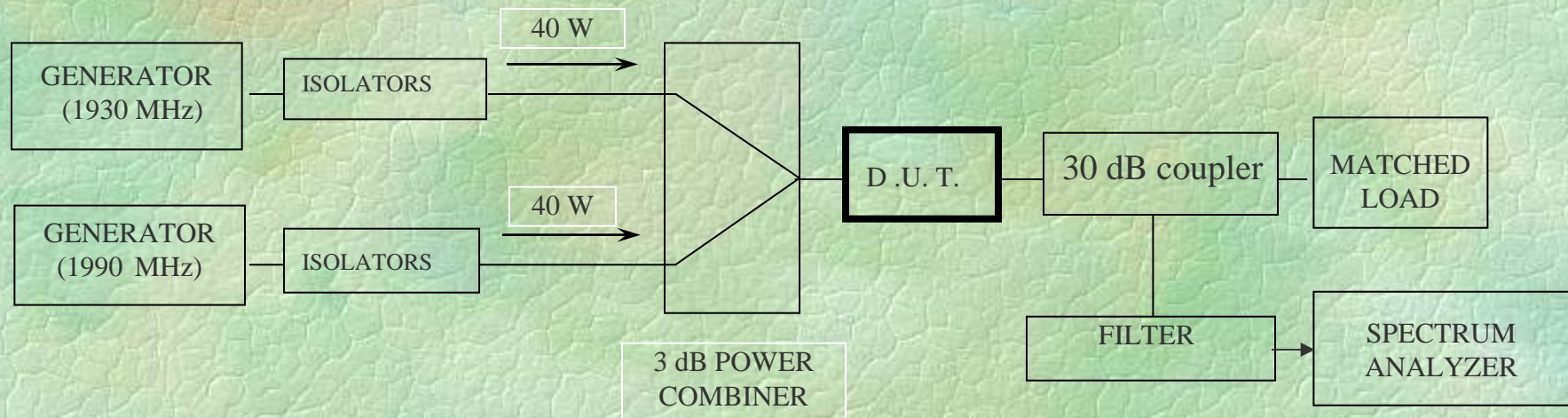
$$\frac{d}{dt} m_z \neq 0$$

## Final Expression

$$m_z = M_s \sqrt{1 - \left(\frac{m_t^2}{M_s}\right)} - M_z \sim \exp(2i\omega t)$$

- **Harmonics due to  $m_t$ 's  $2\omega$  dependence.**
- **When two frequencies co-exists, combined frequencies,  $2\omega_{1,2} \pm \omega_{2,1}$ , develop.**

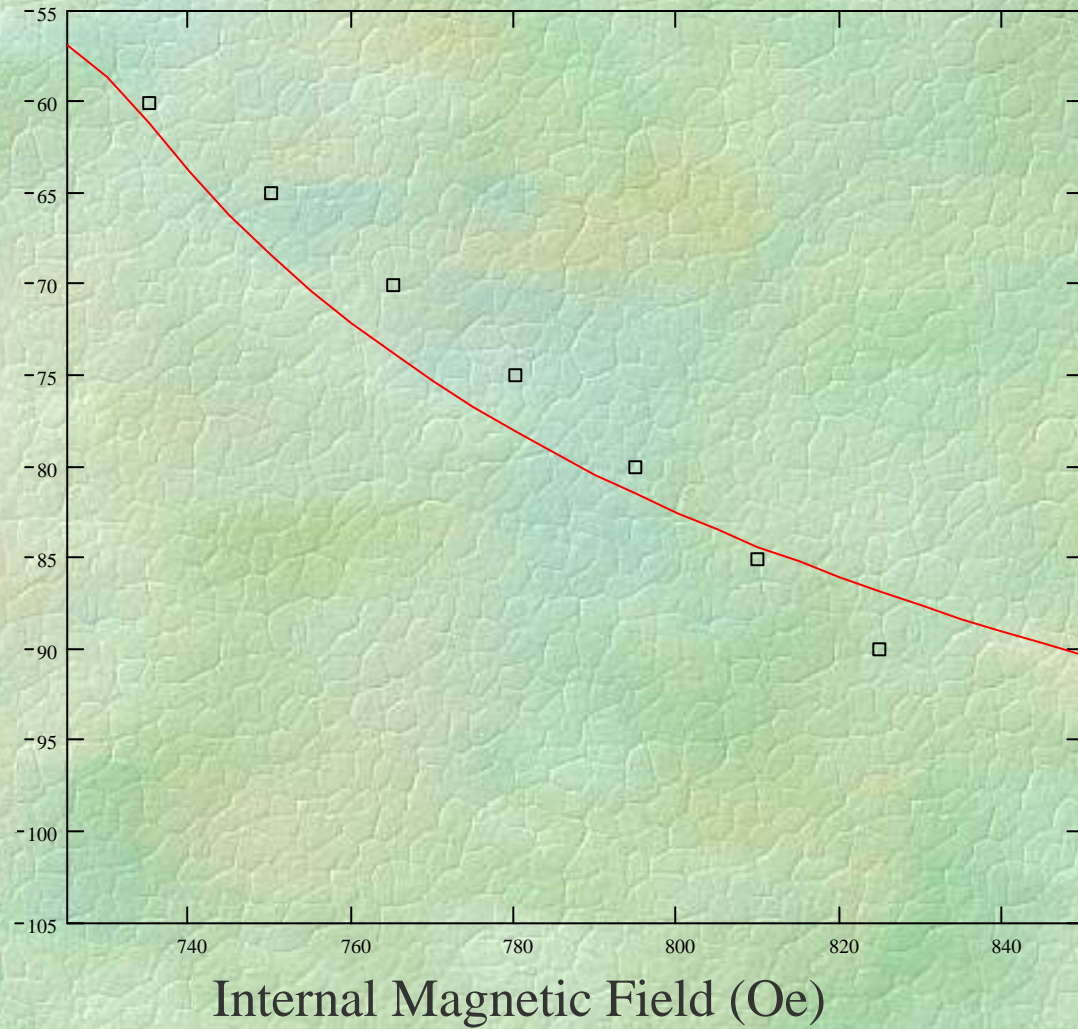
# Experimental Setup



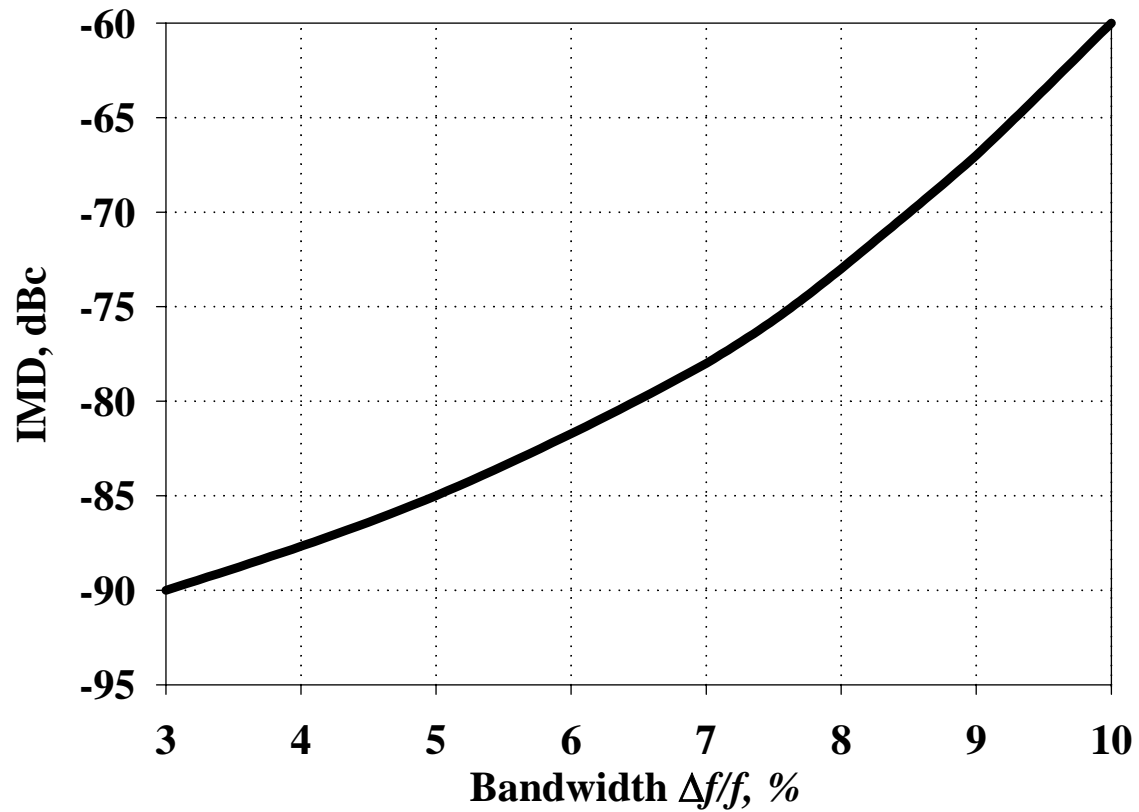
# IMD as a function of field offset



3<sup>rd</sup> order  
Intermodulation  
Distortion  
(dBc)



# IMD vs. Bandwidth



**Bandwidth is Inversely Proportional to the Internal Magnetic Field**

## Summary

- **Intermodulation distortion decreases rapidly as operating field is moved away from resonance - valid for both above resonance and below resonance devices.**
- **Above resonance devices should have better IMD performance than below resonance.**
- **Planar anisotropy shall result in higher intermod values with respect to Isotropic conditions.**